Dingy Output

Tests of Distinguishability and Nonindependence May 19, 2016

1. Text

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Tests of Distinguishability

The focus is to determine whether Gender makes a statistical difference in the data, and if it does, what is that difference. That is, are there differences between Wife and Husband for the mixed variables Self Positivity, Other Postivity, Tension, Satisfaction, and Similar Hobbies and the between-dyads variable Years Married? There are 148 dyads in the sample and no missing data. The analyses employ the method of structural equation modeling using the computer program lavaan. The means and standard deviations of each variable for both Wife and Husband are presented in Table 1. Note that the estimates are maximum likelihood estimates and so the standard deviations are a bit larger than conventional estimates.

There are three ways in which Gender can make a difference. They are differences between the variables in their means, in their variances, and differences between correlations between the two variables. To test if correlations differ, the variances must be set equal for the two members. Note too that the correlations may differ, but cross-variable effects (e.g., actor and partner effects in the Actor-Partner Interdependence Model) might not differ. For instance, the means and variances of Self Positivity might differ for Wife and Husband. For correlation, an example is that the correlations between Self Positivity and Other Postivity might be different for Wife and Husband. Another example is that the correlations between Self Positivity and Years Married might be different for Wife and Husband.

Dingy estimates several models and compares them to determine the best fitting model. To compare models, Dingy uses the chi square test, the chi square difference, the Root Mean Square Error of Approximation or RMSEA, and the Sample Size Adjusted Bayesian Information Criterion or SABIC. With large sample sizes, the chi square tests have so much power that they are almost always statistically significant. Because the sample size for this analysis would not be considered large, the chi square tests may informative. With Dingy, the RMSEA must be less than 0.08 to be considered a good-fitting model. The SABIC is a badness of fit index with smaller values indicating better fit. Its absolute value is not interpretable, but values for different models can be compared. One advantage of the SABIC is that a value can be computed for the model of full distinguishability even though it is a saturated model with zero degrees of freedom. To learn more about these measures of fit go to davidakenny.net/cm/fit.htm (reverse the slashes).

Table 2 provides the measures of fit for five models which allow for different types of distinguishability and Table 3 is a table of the tests of hypotheses of equal means, variances, and correlations. To begin, the test that the means for each variable are equal

(Model I versus Model II) is statistically significant (chi-square(5) = 46.85, p < .001). Thus, there is evidence that the means are unequal. Next, the test of whether the correlations between pairs of variables are equal (Model I versus Model III) is not statistically significant (chi-square(25) = 23.62, p = .541). Thus, the data are consistent with the hypothesis that the correlations are equal, given that the variances are equal. Lastly, the test that the variances are equal (Model IV versus Model V) is not statistically significant (chi-square(5) = 10.34, p = .066). Thus, the data are consistent with the hypothesis that the variances are equal. In terms of chi square tests, the Means Unequal Model or Model II is the best fitting model. In terms of fit indices, the Means Unequal Model or Model II appears to be the best model as it has the lowest value of the RMSEA and the SABIC.

The model of complete indistinguishability is called the I-Sat model by Olsen and Kenny (2006) and that model has a chi square of 80.800 with 35 degrees of freedom. The null model for the indistinguishable case (the model that fixes all correlations to zero, but frees the means and variances and sets them equal across the two members) is 457.624 with 65 degrees of freedom.

Test of Nonindependence

Additionally, the question is whether the scores of the Wife and the Husband are correlated, i.e., nonindependent. There are 25 correlations between the scores of the Wife and the Husband, and the null hypothesis is that these correlations are all zero. The effects due to the between-dyads variables have been removed in tests of nonindependence. Table 4 contains the results from these tests. (Note that SABIC(Sat) refers to the SABIC for the saturated model. Treating dyad members as distinguishable, there is good evidence that there is nonindependence or correlation between the scores of Wife and Husband. Alternatively, if we treat dyad members as indistinguishable, there is good evidence that there is nonindependence or correlation between the scores of Wife and Husband.

2. Tables

Table 1: Descriptive Statistics for Wife and Husband

Person	Wife		Husband	
	Mean	SD	Mean	SD
Self Positivity	4.291	0.408	4.082	0.389
Other Postivity	4.246	0.521	4.281	0.472
Tension	2.520	0.707	2.341	0.653
Satisfaction	3.591	0.528	3.618	0.460
Similar Hobbies	0.189	0.585	-0.034	0.682
Years Married	-0.000	7.694	-0.000	7.694

Table 2: Tests of Different Types of Distinguishability

Model	Equal	Means	Equal	Variances	Equal	Correlations	chi	square	df	р	RMSEA	SABIC
I		Yes		Yes		Yes		80.800	35	<.001	0.094	157.768
II		No		Yes		Yes		33.952	30	.283	0.030	120.083
III		Yes		Yes		No		57.176	10	<.001	0.179	179.959
IV		No		Yes		No		10.344	5	.066	0.085	142.290
V		No		No		No			0			141.109

Table 3: Tests of Hypotheses of Different Types of Distinguishability

Test	chi	square	df	p value
Means I versus II		46.848	5	<.001
Correlations I versus III		23.624	25	.541
Variances IV versus V		10.344	5	.066

Table 4: Tests of Nonindependence across Wife and Husband

	chi	square	df	р	value	RMSEA	SABIC	SABIC(Sat)
Distinguishable		122.044	25		<.001	0.162	217.338	141.109
Indistinguishable		106.455	15		<.001	0.203	155.935	76.968

3. lavaan Output

Test of Distinguishability or the I-SAT Model

lavaan (0.5-16) converged normally after 116 iterations

148
1
ML
80.800
35
0.000

	lhs	op	rhs	label	est	se	z	pvalue
1	SelfPos_H	~1		m1	4.186	0.025	168.056	0.000
2	SelfPos_W	~1		m1	4.186	0.025	168.056	0.000
3	SelfPos_H	~ ~	SelfPos_H	v1	0.170	0.014	12.123	0.000
4	SelfPos_W	~ ~	SelfPos_W	v1	0.170	0.014	12.123	0.000
5	SelfPos_H	~ ~	SelfPos_W		0.014	0.014	1.011	0.312
6	OtherPos_H	~1		m2	4.264	0.032	132.841	0.000
7	OtherPos_W	~1		m2	4.264	0.032	132.841	0.000
8	OtherPos_H	~ ~	OtherPos_H	v2	0.248	0.021	11.852	0.000
9	OtherPos_W	~ ~	OtherPos_W	v2	0.248	0.021	11.852	0.000
10	OtherPos_H	~ ~	OtherPos_W		0.057	0.021	2.744	0.006
11	Tension_H	~1		mЗ	2.431	0.046	53.127	0.000
12	Tension_W	~1		mЗ	2.431	0.046	53.127	0.000
13	Tension_H	~ ~	Tension_H	vЗ	0.471	0.041	11.599	0.000
14	Tension_W	~ ~	Tension_W	vЗ	0.471	0.041	11.599	0.000
15	Tension_H	~ ~	Tension_W		0.149	0.041	3.670	0.000
16	${\tt Satisfaction_H}$	~1		m4	3.605	0.037	98.431	0.000
17	${\tt Satisfaction_W}$	~1		m4	3.605	0.037	98.431	0.000
18	${\tt Satisfaction_H}$	~ ~	${\tt Satisfaction_H}$	v4	0.246	0.024	10.356	0.000

19 Satisfaction_W v4 0.246 0.034 10.356 0.000 20 Satisfaction_H value 0.151 0.024 6.383 0.000 21 SimHob_H -1 m5 0.078 0.042 1.333 0.067 23 SimHob_H SimHob_W v5 0.416 0.036 11.722 0.000 24 SimHob_H SimHob_W v5 0.416 0.036 11.722 0.000 25 SimHob_H SimHob_W v5 0.416 0.036 11.722 0.000 26 SalfPos_H OtherPos_W v12 0.050 0.013 3.988 0.000 28 SalfPos_H OtherPos_W p12 0.050 0.013 3.951 0.000 30 SalfPos_H Tension_H p13<-0.029 0.017 -1.744 0.078 31 SalfPos_H Satisfaction_W p14 0.012 0.007 -1.744 0.081 33 SalfPos_H Satisfaction_H p14 0.037 0.012 3.009 0.003 <th>10</th> <th></th> <th></th> <th></th> <th> 1</th> <th>0.040</th> <th>0 004</th> <th>10 250</th> <th>0 000</th>	10				1	0.040	0 004	10 250	0 000
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41 SelfPos_H ~~ SimHob_H p15 0.016 0.016 1.017 0.309 42 OtherPos_W ~~ Tension_H c23 -0.093 0.022 -4.119 0.000 43 OtherPos_H ~~ Tension_W p23 -0.126 0.022 -5.593 0.000 44 OtherPos_H ~~ Tension_H p23 -0.126 0.022 -5.593 0.000 45 OtherPos_W ~~ Satisfaction_H c24 0.094 0.018 5.354 0.000 46 OtherPos_W ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 47 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 48 OtherPos_H ~~ SimHob_H p25 0.049 0.020 2.488 0.013 51 OtherPos_H ~~ SimHob_H p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H p34 -0.203 0.026 -7.835 0.000 54 Tension_H ~~ Satis	39	SelfPos_H	~ ~	SimHob_W	c15	0.001	0.016	0.067	0.946
42 OtherPos_W ~~ Tension_H c23 -0.093 0.022 -4.119 0.000 43 OtherPos_H ~~ Tension_W c23 -0.093 0.022 -4.119 0.000 44 OtherPos_W ~~ Tension_W p23 -0.126 0.022 -5.593 0.000 45 OtherPos_H ~~ Tension_H p23 -0.126 0.022 -5.593 0.000 46 OtherPos_H ~~ Satisfaction_W c24 0.094 0.018 5.354 0.000 47 OtherPos_W ~~ Satisfaction_W c24 0.014 0.018 6.569 0.000 48 OtherPos_H ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ SimHob_H c25 0.049 0.020 2.488 0.013 51 OtherPos_W ~~ SimHob_W p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 56 Tension_H ~~ S	40	SelfPos_W	~ ~	SimHob_W	p15	0.016	0.016	1.017	0.309
43 OtherPos_H ~~ Tension_W c23 -0.093 0.022 -4.119 0.000 44 OtherPos_W ~~ Tension_W p23 -0.126 0.022 -5.593 0.000 45 OtherPos_H ~~ Tension_H p23 -0.126 0.022 -5.593 0.000 46 OtherPos_W ~~ Satisfaction_H c24 0.094 0.018 5.354 0.000 47 OtherPos_H ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 48 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 51 OtherPos_H ~~ SimHob_W c25 0.049 0.020 2.488 0.013 52 OtherPos_H ~~ SimHob_H p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H c34 -0.139 0.026 -5.380 0.000 54 Tension_H ~~ <t< td=""><td>41</td><td>SelfPos_H</td><td>~ ~</td><td>SimHob_H</td><td>p15</td><td>0.016</td><td>0.016</td><td>1.017</td><td>0.309</td></t<>	41	SelfPos_H	~ ~	SimHob_H	p15	0.016	0.016	1.017	0.309
44 OtherPos_W ~~ Tension_W p23 -0.126 0.022 -5.593 0.000 45 OtherPos_H ~~ Tension_H p23 -0.126 0.022 -5.593 0.000 46 OtherPos_W ~~ Satisfaction_H c24 0.094 0.018 5.354 0.000 47 OtherPos_H ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 48 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 49 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 52 OtherPos_H ~~ SimHob_H p25 0.049 0.020 2.488 0.013 51 OtherPos_H ~~ SimHob_H p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H p24 -0.139 0.026 -5.380 0.000 55 Tension_H ~~ Satisfaction_W p34 -0.203 0.027 -1.545 0.122 59 <td>42</td> <td>OtherPos_W</td> <td>~ ~</td> <td>Tension_H</td> <td>c23</td> <td>-0.093</td> <td>0.022</td> <td>-4.119</td> <td>0.000</td>	42	OtherPos_W	~ ~	Tension_H	c23	-0.093	0.022	-4.119	0.000
45 OtherPos_H ~~ Tension_H p23 -0.126 0.022 -5.593 0.000 46 OtherPos_W ~~ Satisfaction_H c24 0.094 0.018 5.354 0.000 47 OtherPos_H ~~ Satisfaction_W p24 0.116 0.018 5.354 0.000 48 OtherPos_H ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 49 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 51 OtherPos_H ~~ SimHob_H c25 0.049 0.020 2.488 0.013 52 OtherPos_H ~~ SimHob_H p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H p25 0.057 0.026 -5.380 0.000 55 Tension_H ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 58 Tension_H ~~	43	OtherPos_H	~ ~	Tension_W	c23	-0.093	0.022	-4.119	0.000
45 OtherPos_H ~~ Tension_H p23 -0.126 0.022 -5.593 0.000 46 OtherPos_W ~~ Satisfaction_H c24 0.094 0.018 5.354 0.000 47 OtherPos_H ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 48 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ SimHob_H c25 0.049 0.020 2.488 0.013 51 OtherPos_H ~~ SimHob_H p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H p25 0.057 0.026 -5.380 0.000 55 Tension_H ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 58 Tension_H ~~	44	—			p23	-0.126	0.022		
46 OtherPos_W ~~ Satisfaction_H c24 0.094 0.018 5.354 0.000 47 OtherPos_H ~~ Satisfaction_W c24 0.094 0.018 5.354 0.000 48 OtherPos_H ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 49 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_H ~~ Satisfaction_H c25 0.049 0.020 2.488 0.013 51 OtherPos_H ~~ SimHob_W c25 0.049 0.020 2.488 0.013 52 OtherPos_H ~~ SimHob_W p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H c34 -0.139 0.026 -5.380 0.000 55 Tension_H ~~ Satisfaction_H p34 -0.203 0.026 -7.835 0.000 56 Tension_H ~~ SimHob_W c35 -0.042 0.027 -1.545 0.122 59 <td>45</td> <td>_</td> <td></td> <td>_</td> <td>p23</td> <td>-0.126</td> <td>0.022</td> <td>-5.593</td> <td>0.000</td>	45	_		_	p23	-0.126	0.022	-5.593	0.000
47 OtherPos_H ~~ Satisfaction_W c24 0.094 0.018 5.354 0.000 48 OtherPos_W ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 49 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_W ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 51 OtherPos_H ~~ Satisfaction_H c25 0.049 0.020 2.488 0.013 52 OtherPos_H ~~ SimHob_W p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H c34 -0.139 0.026 -5.380 0.000 54 Tension_H ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 55 Tension_H ~~ Satisfaction_H p34 -0.203 0.026 -7.835 0.000 58 Tension_H ~~ Satisfaction_H p34 -0.203 0.026 -7.835 0.122 59 Tension_H ~~ SimHob_H c35 -0.042 0.027 -1.545 0.122 <		—			-				
48 OtherPos_W ~~ Satisfaction_W p24 0.116 0.018 6.569 0.000 49 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_W ~~ SimHob_H c25 0.049 0.020 2.488 0.013 51 OtherPos_H ~~ SimHob_W c25 0.049 0.020 2.488 0.013 52 OtherPos_H ~~ SimHob_W p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ Satisfaction_H c34 -0.139 0.026 -5.380 0.000 54 Tension_W ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 55 Tension_H ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 58 Tension_H ~~ SimHob_H c35 -0.042 0.027 -1.545 0.122 59 Tension_H ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 61 Tension_H ~~ SimHob_H p45 0.092 0.021 3.385 0.001 63 Sati		—				0.094	0.018		0.000
49 OtherPos_H ~~ Satisfaction_H p24 0.116 0.018 6.569 0.000 50 OtherPos_W ~~ SimHob_H c25 0.049 0.020 2.488 0.013 51 OtherPos_H ~~ SimHob_W c25 0.049 0.020 2.488 0.013 52 OtherPos_H ~~ SimHob_W p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ SimHob_H p25 0.057 0.020 2.899 0.000 54 Tension_W ~~ Satisfaction_H c34 -0.139 0.026 -5.380 0.000 55 Tension_H ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 56 Tension_H ~~ Satisfaction_H p34 -0.203 0.026 -7.835 0.000 58 Tension_H ~~ SimHob_H c35 -0.042 0.027 -1.545 0.122 59 Tension_H ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 61 Tension_H ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 62 Satisfact		_		_			0.018		
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52 OtherPos_W ~~ SimHob_W p25 0.057 0.020 2.899 0.004 53 OtherPos_H ~~ SimHob_H p25 0.057 0.020 2.899 0.004 54 Tension_W ~~ Satisfaction_H c34 -0.139 0.026 -5.380 0.000 55 Tension_H ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 56 Tension_H ~~ Satisfaction_H p34 -0.203 0.026 -7.835 0.000 57 Tension_H ~~ Satisfaction_H p34 -0.203 0.027 -1.545 0.122 59 Tension_H ~~ Satisfaction_H p35 -0.042 0.027 -1.981 0.048 61 Tension_H ~~ SimHob_W p35 -0.054 0.027 -1.981 0.048 62 Satisfaction_W ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 63 Satisfaction_W ~~ SimHob_H p45 0.022 0.021 4.313 0.000 64 Satisfaction_H ~~ <td></td> <td>_</td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td> <td></td>		_							
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56 Tension_W ~~ Satisfaction_W p34 -0.203 0.026 -7.835 0.000 57 Tension_H ~~ Satisfaction_H p34 -0.203 0.026 -7.835 0.000 58 Tension_W ~~ SimHob_H c35 -0.042 0.027 -1.545 0.122 59 Tension_H ~~ SimHob_W c35 -0.042 0.027 -1.545 0.122 60 Tension_H ~~ SimHob_W p35 -0.054 0.027 -1.981 0.048 61 Tension_H ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 62 Satisfaction_W ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 63 Satisfaction_W ~~ SimHob_H c45 0.072 0.021 3.385 0.001 64 Satisfaction_W ~~ SimHob_W p45 0.092 0.021 4.313 0.000 65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~2 yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc11 0.230 0.193 1.192 0.233 70 OtherPos_W ~~ yearsmar cc12 0.506 0.250		-		-					
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59 Tension_H ~~ SimHob_W c35 -0.042 0.027 -1.545 0.122 60 Tension_W ~~ SimHob_W p35 -0.054 0.027 -1.981 0.048 61 Tension_H ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 62 Satisfaction_W ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 63 Satisfaction_W ~~ SimHob_H c45 0.072 0.021 3.385 0.001 64 Satisfaction_W ~~ SimHob_W c45 0.092 0.021 4.313 0.000 65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~2 yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_H ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc12 0		-		-	-				
60 Tension_W ~~ SimHob_W p35 -0.054 0.027 -1.981 0.048 61 Tension_H ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 62 Satisfaction_W ~~ SimHob_H c45 0.072 0.021 3.385 0.001 63 Satisfaction_H ~~ SimHob_W c45 0.072 0.021 3.385 0.001 64 Satisfaction_W ~~ SimHob_W p45 0.092 0.021 4.313 0.000 65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~2 yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 70 OtherPos_W ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.		_							
61 Tension_H ~~ SimHob_H p35 -0.054 0.027 -1.981 0.048 62 Satisfaction_W ~~ SimHob_H c45 0.072 0.021 3.385 0.001 63 Satisfaction_H ~~ SimHob_W c45 0.072 0.021 3.385 0.001 64 Satisfaction_W ~~ SimHob_W p45 0.092 0.021 4.313 0.000 65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~ yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		-							
62 Satisfaction_W ~~ SimHob_H c45 0.072 0.021 3.385 0.001 63 Satisfaction_H ~~ SimHob_W c45 0.072 0.021 3.385 0.001 64 Satisfaction_H ~~ SimHob_W p45 0.092 0.021 4.313 0.000 65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~~ yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		—			-				
63 Satisfaction_H ~~ SimHob_W c45 0.072 0.021 3.385 0.001 64 Satisfaction_W ~~ SimHob_W p45 0.092 0.021 4.313 0.000 65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~~ yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043 70 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		_		_	-				
64 Satisfaction_W ~~ SimHob_W p45 0.092 0.021 4.313 0.000 65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~~ yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043									
65 Satisfaction_H ~~ SimHob_H p45 0.092 0.021 4.313 0.000 66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~~ yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043 70 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		—		_					
66 yearsmar ~1 mm1 0.000 0.632 0.000 1.000 67 yearsmar ~~ yearsmar vv1 59.192 6.881 8.602 0.000 68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc11 0.230 0.193 1.192 0.233 70 OtherPos_W ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		—		-	-				
67yearsmar ~~yearsmarvv159.1926.8818.6020.00068SelfPos_W ~~yearsmarcc110.2300.1931.1920.23369SelfPos_H ~~yearsmarcc110.2300.1931.1920.23370OtherPos_W ~~yearsmarcc120.5060.2502.0200.04371OtherPos_H ~~yearsmarcc120.5060.2502.0200.043		_			-				
68 SelfPos_W ~~ yearsmar cc11 0.230 0.193 1.192 0.233 69 SelfPos_H ~~ yearsmar cc11 0.230 0.193 1.192 0.233 70 OtherPos_W ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		•							
69 SelfPos_H ~~ yearsmar cc11 0.230 0.193 1.192 0.233 70 OtherPos_W ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		•		•					
70 OtherPos_W ~~ yearsmar cc12 0.506 0.250 2.020 0.043 71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		_		v					
71 OtherPos_H ~~ yearsmar cc12 0.506 0.250 2.020 0.043		_		v					
		_		-					
(2 lension_W ~~ yearsmar cc13 -0.587 0.355 -1.651 0.099		_		-					
	72	Tension_W	~ ~	yearsmar	cc13	-0.587	0.355	-1.651	0.099

70	Π		_		1 0	0 507	0 955	1 051	0 000
73		sion_H ~~	-	vearsmar		-0.587		-1.651	0.099
	Satisfact Satisfact	—	-	vearsmar		-0.022		-0.080 -0.080	0.936
76		_	-	vearsmar		-0.022		-0.080 -1.416	0.936 0.157
70		nHob_W ~~ nHob_H ~~	-	vearsmar vearsmar		-0.465		-1.410 -1.416	0.157
11		ci.upper	-		0010	0.405	0.520	1.410	0.157
1									
1 2	4.138		4.186	10.167					
2 3	4.138		4.186						
3 4	0.142	0.197		1.000					
4 5	0.142	0.197	0.170	1.000					
5 6	-0.013	0.042	0.014	0.083 8.568					
6 7	4.201	4.326	4.264						
8	4.201	4.326		8.568					
	0.207	0.289		1.000					
9	0.207	0.289		1.000					
10	0.016	0.098	0.057	0.232					
11	2.341	2.520	2.431	3.543					
12	2.341	2.520		3.543					
13	0.391	0.550		1.000					
14	0.391	0.550	0.471	1.000					
15	0.069	0.228	0.149	0.316					
16	3.533	3.677	3.605	7.274					
17	3.533	3.677	3.605	7.274					
18	0.199	0.292	0.246	1.000					
19	0.199	0.292	0.246	1.000					
20	0.105	0.198	0.151	0.616					
21	-0.005	0.161	0.078	0.120					
22		0.161	0.078	0.120					
23	0.347		0.416	1.000					
24	0.347		0.416	1.000					
25	0.046	0.185		0.278					
26	0.025	0.074		0.242					
27	0.025	0.074	0.050	0.242					
28	0.025	0.075	0.050	0.245					
29	0.025	0.075	0.050	0.245					
30	-0.063		-0.030	-0.105					
31	-0.063		-0.030	-0.105					
32			-0.029	-0.104					
33			-0.029	-0.104 0.060					
34 35		0.037		0.060					
		0.037							
36		0.061	0.037	0.182					
37	0.013	0.061	0.037	0.182					
38	-0.030 -0.030	0.032		0.004					
39		0.032		0.004					
40	-0.015	0.047		0.060					
41 42	-0.015 -0.137	0.047	0.016	0.060					
42				-0.271					
43			-0.093	-0.271					
44			-0.126	-0.368					
45 46			-0.126	-0.368					
46		0.129		0.382					
47 48		0.129	0.094	0.382					
48	0.081	0.150	0.116	0.469					

49	0.081	0.150	0.116	0.469
50	0.010	0.088	0.049	0.153
51	0.010	0.088	0.049	0.153
52	0.019	0.096	0.057	0.178
53	0.019	0.096	0.057	0.178
54	-0.190	-0.089	-0.139	-0.410
55	-0.190	-0.089	-0.139	-0.410
56	-0.254	-0.152	-0.203	-0.597
57	-0.254	-0.152	-0.203	-0.597
58	-0.095	0.011	-0.042	-0.095
59	-0.095	0.011	-0.042	-0.095
60	-0.107	-0.001	-0.054	-0.121
61	-0.107	-0.001	-0.054	-0.121
62	0.030	0.113	0.072	0.225
63	0.030	0.113	0.072	0.225
64	0.050	0.133	0.092	0.286
65	0.050	0.133	0.092	0.286
66	-1.240	1.239	0.000	0.000
67	45.705	72.678	59.192	1.000
68	-0.148	0.607	0.230	0.072
69	-0.148	0.607	0.230	0.072
70	0.015	0.997	0.506	0.132
71	0.015	0.997	0.506	0.132
72	-1.283	0.110	-0.587	-0.111
73	-1.283	0.110	-0.587	-0.111
74	-0.575	0.530	-0.022	-0.006
75	-0.575	0.530	-0.022	-0.006
76	-1.108	0.179	-0.465	-0.094
77	-1.108	0.179	-0.465	-0.094